

EXPLICIT FABER POLYNOMIALS ON CIRCULAR SECTORS

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ABSTRACT. We present explicit and precise expressions for the Faber polynomials on circular sectors up to degree 20. The precision is obtained by modifying (and simultaneously speeding up) an algorithm of Coleman and Smith so that an essential part of the Faber polynomials can be represented using only rational numbers. The growth of the coefficients of the Faber polynomials is determined. In addition, explicit expressions are given for the area two-norm and line two-norm of these polynomials. A conjecture is stated with respect to the uniform (infinity) norm which would also allow the explicit computation of the corresponding uniform norms of the Faber polynomials. Apart from a table of Faber polynomials, there are several other tables and graphs that illustrate the behavior of the Faber polynomials.

1. INTRODUCTION

Let $S \subset \mathbb{C}$ be a compact set whose complement admits a conformal mapping φ onto the exterior of a compact disk D . One may assume that the disk is centered at the origin and also that φ is *normalized* by the condition

$$(1.1) \quad \varphi'(\infty) = \lim_{z \rightarrow \infty} \frac{\varphi(z)}{z} = 1.$$

This condition makes the mapping φ as well as the radius ρ of D unique. The radius ρ is called the *transfinite diameter* or the *capacity* of S . For its properties see Gaier [6, p. 136].

The normalized mapping φ has an expansion of the form

$$(1.2) \quad \varphi(z) = z + a_0 + \frac{a_1}{z} + \dots,$$

and thus

$$(1.3) \quad (\varphi(z))^n = z^n + f_{n,n-1}z^{n-1} + \dots + f_{n,0} + \frac{f_{n,-1}}{z} + \frac{f_{n,-2}}{z^2} + \dots$$

with certain coefficients $f_{n,j}$, $j = n-1, n-2, \dots, 0, -1, -2, \dots$, which could be computed from a_0, a_1, \dots .

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The polynomial occurring in (1.3), namely

$$(1.4) \quad F_n(z) = z^n + f_{n,n-1}z^{n-1} + \cdots + f_{n,0},$$

is called the n th *Faber polynomial* of S . These polynomials are attractive because, roughly speaking, they have good approximation power. Some estimates are given in §3.3. For more explicit properties of Faber polynomials, we refer to Gaier [7, Chapter I, §6].

The explicit construction of the Faber polynomials of a given set S depends essentially on the knowledge of the conformal mapping φ . For *circular sectors*, Coleman and Smith [1] were able to construct the necessary conformal mapping via Schwarz-Christoffel and some other auxiliary mappings. By using a general recursion for Faber polynomials, the result of Coleman and Smith was a set of recursions which ultimately yielded the Faber polynomials. The origin of the general recursion for Faber polynomials (appearing in the sequel as Step 4 of the Coleman and Smith algorithm) is unknown to us. However, it is stated and used by Kövari and Pommerenke [9, p. 195]. A statement, including a derivation, is contained in a paper by Curtiss [3, p. 578]. The importance for numerical purposes has been stressed by Ellacott [4, p. 578].

However, this set of recursions is rather involved, so that there is hardly any chance to compute manually and explicitly the Faber polynomials for larger values of n . Thus, Coleman and Smith presented these polynomials explicitly only up to degree three. Beyond that, they used their recursions to compute numerically the coefficients of the Faber polynomials F_n for $n \leq 15$ for six selected opening angles of the sector, to 14 decimals precision (Coleman and Smith [2]).

By simplifying the recursions, and by using symbolic computation, we show that it is practical to generate the Faber polynomials explicitly in terms of the opening angle to almost any degree. The symbolic computation systems we have used, and their limitations, are discussed at the end of the paper.

We also make use of another property that was at least indicated by Coleman and Smith [1, p. 238]. If we compare the coefficients that are in corresponding position in the F_n , as a function of the degree n , we see that they are the values of a certain polynomial. In consequence, the first terms of F_n can be given explicitly for *all* n . We will explain this property later.

We mention another family of polynomials that are also defined with respect to the given compact set S , namely the *Chebyshev polynomials* T_n . A *monic* polynomial $T_n(z) = z^n + a_{n,n-1}z^{n-1} + \cdots + a_{n,0}$ is a Chebyshev polynomial if it has minimal uniform norm on S among all monic complex polynomials of the same degree. Formally, this can be stated as

$$(1.5) \quad \|T_n\|_\infty = \max_{z \in S} |T_n(z)| \leq \|P_n\|_\infty \quad \text{for all } P_n \in \Pi_n,$$

where all polynomials are monic.

We will use the notation Π_n for the set of all polynomials up to degree n over \mathbb{K} , where $\mathbb{K} = \mathbb{C}$ or $\mathbb{K} = \mathbb{R}$. The definition of Chebyshev polynomials implies for the Faber polynomials F_n that

$$(1.6) \quad \|T_n\|_\infty \leq \|F_n\|_\infty.$$

If S is a disk or an interval, the polynomials F_n and T_n coincide. For the unit disk we have $F_n(z) = T_n(z) = z^n$ and $\|F_n\|_\infty = 1$. For the interval

$S = [0, 1]$ we have

$$F_n(z) = T_n(z) = 2^{1-2n} \cos(n \arccos(2z - 1)),$$

and thus $\|F_n\|_\infty = 2^{1-2n}$ for $n > 0$. In the latter case, the F_n coincide with the ordinary Chebyshev polynomials adjusted to the interval $[0, 1]$ and scaled so that the leading coefficient is one. We will consider how to compute the norms of Faber polynomials in §3. Further results on Faber polynomials can be found in Ellacott [5].

2. COMPUTATION OF FABER POLYNOMIALS FOR CIRCULAR SECTORS

Since the recursion formulae were derived by Coleman and Smith, we only describe those steps necessary to derive Faber polynomials for circular sectors

$$(2.1) \quad S = S_\alpha = \{z \in \mathbb{C} : |z| \leq 1, |\arg z| \leq \alpha\},$$

where $0 \leq \alpha \leq \pi$. The opening angle of the sector is 2α . The transfinite diameter of S_α , as given by Coleman and Smith, is

$$(2.2) \quad \rho = \begin{cases} 1/(2 - \alpha/\pi)^2 \{(\pi/\alpha)(2 - \alpha/\pi)\}^{\alpha/\pi} & \text{for } \alpha \neq 0, \\ 0.25 & \text{for } \alpha = 0. \end{cases}$$

The computational procedure for finding the Faber polynomials F_n accounts for the geometry of S_α by means of x , where

$$(2.3) \quad x = 1 - 2c, \quad c = \frac{\alpha}{\pi} \left(2 - \frac{\alpha}{\pi}\right).$$

For a given S_α we do the following steps:

Step 1. Compute Legendre polynomials P and polynomials a :

$$\begin{aligned} P_0(x) &= 1; & P_1(x) &= x; \\ (n + 1)P_{n+1}(x) - (2n + 1)xP_n(x) + nP_{n-1}(x) &= 0, & n > 0; \\ a_0 &= 1; & a_n(x) &= P_n(x) + P_{n-1}(x), \quad n > 0; \end{aligned}$$

Step 2. Compute coefficients β of the Laurent expansion:

$$\begin{aligned} \beta_0(x) &= a_1(x) = 1 + x; \\ (n + 1)\beta_n(x) &= a_{n+1}(x) - \sum_{k=1}^{n-1} k\beta_k(x)a_{n-k}(x), & n > 0; \end{aligned}$$

Step 3. Define b by multiplying β with powers of the transfinite diameter ρ :

$$b_n(x) = \beta_n(x)\rho^{n+1}, \quad n \geq 0;$$

Step 4. Compute Faber polynomials F and replace x by $1 - 2c$:

$$\begin{aligned} F_0(z) &= 1; & F_1(z) &= z - b_0(x); \\ F_{n+1}(z) &= (z - b_0(x))F_n(z) - \sum_{k=1}^{n-1} b_k(x)F_{n-k}(z) \\ &\quad - (1 + n)b_n(x), & n > 0. \end{aligned}$$

Observe that c increases from 0 to 1 and ρ increases from 0.25 to 1 as α increases from 0 to π . Apart from small notational differences, Coleman and Smith’s computation is the same. However, we can make some simplifications. When $\alpha = \pi$, the n th Faber polynomial reduces to z^n , which is reflected by $c - 1 = 0$, or, equivalently, by $x + 1 = 0$. Therefore, the Faber polynomial F_n must have the form $F_n(z) = z^n + (1 - c)\pi_{n-1}(z)$, where $\pi_{n-1} \in \Pi_{n-1}$. Furthermore, we can eliminate the transfinite diameter ρ by observing that

$$(2.4) \quad F_n(z\rho) = \rho^n(z^n + (1 - c)(p_{n-1,0}z^{n-1} + p_{n-1,1}z^{n-2} + \cdots + p_{n-1,n-1})), \quad n > 0.$$

This follows from Steps 3 and 4. We use the following notation:

$$(2.5) \quad \begin{aligned} \Phi_0 &= 1; \\ \Phi_n(z) &= z^n + (1 - c)(p_{n-1,0}z^{n-1} + p_{n-1,1}z^{n-2} + \cdots + p_{n-1,n-1}), \end{aligned} \quad n > 0,$$

where Φ_n is now independent of ρ and the coefficients $p_{n-1,j} \in \Pi_j$, $j = 0, 1, \dots, n - 1$, are polynomials in the variable c . The geometric meaning of c is given in (2.3). The polynomials

$$(2.6) \quad \tilde{F}_n(z) = F_n(z)\rho^{-n} = \Phi_n(z/\rho)$$

are the *scaled* Faber polynomials.

Now it is easy to see that the functions Φ_n obey the same recursion as the functions F_n in Step 4, after the b ’s are replaced with the β ’s. Thus, computing Φ_n rather than F_n eliminates Step 3. But we can do better. Since the polynomial factor of $1 - c$ in (2.5) contains already all the essential information about Φ_n , we derive a recursion for this factor. For $c < 1$, we denote the factor by

$$(2.7) \quad \phi_{n-1}(z) = p_{n-1,0}z^{n-1} + p_{n-1,1}z^{n-2} + \cdots + p_{n-1,n-1}, \quad n > 0,$$

which changes (2.5) to

$$(2.5') \quad \Phi_0 = 1; \quad \Phi_n(z) = z^n + (1 - c)\phi_{n-1}(z), \quad n > 0.$$

In terms of the newly introduced ϕ_{n-1} , the recursion of Step 4 reads:

$$(2.8a) \quad \phi_0 = -2; \quad \tilde{\beta}_k = \beta_k/(1 - c),$$

$$(2.8b) \quad \begin{aligned} \phi_n &= (z - \beta_0)\phi_{n-1} - \sum_{k=1}^{n-1} \beta_k\phi_{n-k-1} \\ &- \sum_{k=0}^{n-1} \tilde{\beta}_k z^{n-k} - (n + 1)\tilde{\beta}_n, \end{aligned} \quad n > 0.$$

Since $a_n(-1) = P_n(-1) + P_{n-1}(-1) = 0$, where $n > 0$, all polynomials a have the factor $x + 1$, or, equivalently, the factor $1 - c$. The same applies to the polynomials β_n , as is evident from Step 2. Therefore, by one sweep of the Horner scheme at $x = -1$ or at $c = 1$, this factor can be cancelled, thus obtaining $\tilde{\beta}_k = \beta_k/(1 - c)$.

It is unreasonable to work with the two closely related geometric quantities x and c simultaneously. Therefore, we delete x and work with c only. Since the

Legendre polynomials are only used to generate the polynomials a , they need not be stored. In the following algorithm we assume that we want to compute all Faber polynomials up to a certain degree $n_{\max} > 1$. We replace the above steps by

Algorithm. Apply simplifications, compute ϕ_n :

A. Initialization:

$$P_0 = 1; P_1 = 1 - 2c; \phi[0] = -2; \\ a[1] = 2 - 2c; \beta[0] = 2 - 2c; \tilde{\beta}[0] = 2;$$

B. For $n = 1$ to $n_{\max} - 1$ compute

$$P_2 = ((2n + 1)(1 - 2c)P_1 - nP_0)/(n + 1);$$

$$P_0 = P_1; P_1 = P_2;$$

$$a[n + 1] = P_0 + P_1;$$

$$\beta[n] = (a[n + 1] - \sum_{k=1}^{n-1} k\beta[k]a[n - k])/(n + 1); \tilde{\beta}[n] = \beta[n]/(1 - c);$$

$$\phi[n] = z\phi[n - 1] - (n + 1)\tilde{\beta}[n] - \sum_{k=0}^{n-1} (\beta[k]\phi[n - k - 1] + \tilde{\beta}[k]z^{n-k});$$

print polynomial coefficients of $\phi[n]$; measure the computing time;

$$\Phi[n + 1] = z^{n+1} + (1 - c)\phi[n]; \{\text{may be deleted}\}$$

$$F[n + 1](z) = \rho^{n+1}\Phi[n + 1](z/\rho). \{\text{may be deleted}\}$$

Example. We compute the quantities necessary to generate the Faber polynomials F_n and the polynomials ϕ_{n-1} for $n \leq 4$. We do not list the Φ_n , since they are immediate from ϕ_{n-1} and (2.5').

Step 1. $P_0 = 1; P_1(x) = x; P_2(x) = \frac{1}{2}(-1 + 3x^2); P_3(x) = \frac{1}{2}(-3x + 5x^3);$
 $P_4(x) = \frac{1}{8}(3 - 30x^2 + 35x^4); a_0 = 1; a_1(x) = 1 + x; a_2(x) = \frac{1}{2}(-1 + 2x + 3x^2);$
 $a_3(x) = \frac{1}{2}(-1 - 3x + 3x^2 + 5x^3); a_4(x) = \frac{1}{8}(3 - 12x - 30x^2 + 20x^3 + 35x^4);$

Step 2. $\beta_0(x) = 1 + x; \beta_1(x) = \frac{1}{4}(-1 + 2x + 3x^2); \beta_2(x) = \frac{1}{12}(-1 - 7x + x^2 + 7x^3);$
 $\beta_3(x) = \frac{1}{48}(5 + 4x - 30x^2 - 4x^3 + 25x^4);$

Step 3. $b_n = \rho^{n+1}\beta_n;$

Step 4. $F_0 = 1; F_1(z) = z - \rho(1 + x); F_2(z) = z^2 - 2\rho(1 + x)z + \frac{1}{2}\rho^2(3 + 2x - x^2);$
 $F_3(z) = z^3 - 3\rho(1 + x)z^2 + \frac{3}{4}\rho^2(5 + 6x + x^2)z - \frac{1}{2}\rho^3(3 + x - x^2 + x^3); F_4(z)$
 $= z^4 - 4\rho(1 + x)z^3 + \rho^2(7 + 10x + 3x^2)z^2 - \frac{1}{3}\rho^3(17 + 23x + 7x^2 + x^3)z +$
 $\frac{1}{8}\rho^4(11 + 4x + 2x^2 + 4x^3 - 5x^4).$

Algorithm. $a_1(c) = 2 - 2c; a_2(c) = 2 - 8c + 6c^2; a_3(c) = 2 - 18c + 36c^2 - 20c^3;$
 $a_4(c) = 2 - 32c + 120c^2 - 160c^3 + 70c^4;$

$$\tilde{\beta}_0 = 2; \tilde{\beta}_1(c) = 1 - 3c; \tilde{\beta}_2(c) = -8/3c + 14/3c^2; \tilde{\beta}_3(c) = -4/3c + 23/3c^2 - 25/3c^3;$$

$$\phi_0 = -2; \phi_1(z) = -4z + 2(1 + c); \phi_2(z) = -6z^2 + 3(3 - c)z - 2(1 + 2c^2);$$

$$\phi_3(z) = -8z^3 + 4(5 - 3c)z^2 + (-16 + \frac{32}{3}c - \frac{8}{3}c^2)z + 2(1 + c - 3c^2 + 5c^3).$$

In order to make the structure of the coefficients $p_{n-1,j}$ defined in (2.5) more explicit, we show their dependence on n . For $n \geq 0$, for $j = 0, 1, \dots, n$, and for $s = j(j + 1)/2 + 1$, we define

$$(2.9) \quad p_{n,j}(c) = \gamma_{n+1,s} + \gamma_{n+1,s+1}c + \dots + \gamma_{n+1,s+j}c^j.$$

Therefore, the coefficients $\gamma_{n+1,k}$ may be regarded as the elements in row $n + 1$ of a matrix

$$(2.10) \quad \Gamma = (\gamma_{jk}), \quad j = 1, 2, \dots; \quad k = 1, 2, \dots, j(j + 1)/2,$$

which has infinitely many rows. Row j is finite with $j(j + 1)/2$ elements. As an example, we put the above ϕ_3 into the form of notation (2.9) and obtain

$$\begin{aligned} \phi_3(z) &= -8z^3 + 4(5 - 3c)z^2 + (-16 + \frac{32}{3}c - \frac{8}{3}c^2)z + 2(1 + c - 3c^2 + 5c^3) \\ &= p_{30}(c)z^3 + p_{31}(c)z^2 + p_{32}(c)z + p_{33} \\ &= \gamma_{41}z^3 + (\gamma_{42} + \gamma_{43}c)z^2 + (\gamma_{44} + \gamma_{45}c + \gamma_{46}c^2)z \\ &\quad + \gamma_{47} + \gamma_{48}c + \gamma_{49}c^2 + \gamma_{4,10}c^3. \end{aligned}$$

We denote the submatrix of Γ consisting of the first n rows by

$$(2.11) \quad \Gamma_n = (\gamma_{jk}), \quad j = 1, 2, \dots, n; \quad k = 1, 2, \dots, j(j + 1)/2.$$

Theorem 1. *All entries of the matrix Γ are rational.*

Proof. Immediate from Steps 1–4 and (2.4), (2.9). \square

In Table 5 of the appendix (see supplement section at the end of this issue), we list the polynomials $p_{n-1,j}$ for $j = 0(1)n - 1$ and $n = 1(1)20$. Compare also (2.9). The polynomials $p_{n-1,j}$ define the polynomials $\phi_{n-1}(z) = \sum_{j=0}^{n-1} p_{n-1,j} z^{n-j-1}$. The polynomials $\phi_{n-1}(z)$ define the polynomials $\Phi_n(z)$ (compare (2.5)). In turn, the polynomials $\Phi_n(z)$ define the Faber polynomials $F_n(z)$ (compare (2.6) and (2.2)).

If we were to store all coefficients for degrees up to n , we would need $1 + 3 + 6 + \dots + 0.5n(n + 1) = n(n + 1)(n + 2)/6$ storage locations. For $n = 5, 10, 15, 20$, and 100 , these numbers are $35, 220, 680, 1540$, and 171700 , respectively. In comparison, Coleman and Smith [2] required 628 numerical coefficients for the coefficients of the Faber polynomials up to degree 15 on only six selected opening angles.

From Table 5 of the appendix we have

$$(2.12) \quad \Gamma_{10} = \begin{pmatrix} -2 & & & & & & & & & & \\ -4 & 2 & 2 & & & & & & & & \\ -6 & 9 & -3 & -2 & 0 & -4 & & & & & \\ -8 & 20 & -12 & -16 & \frac{32}{3} & -\frac{8}{3} & 2 & 2 & -6 & 10 & \\ -10 & 35 & -25 & -50 & \frac{160}{3} & -\frac{40}{3} & 25 & -\frac{65}{3} & \frac{10}{3} & \frac{10}{3} & \dots \\ -12 & 54 & -42 & -112 & 144 & -44 & 105 & -151 & 65 & -7 & \dots \\ -14 & 77 & -63 & -210 & \frac{896}{3} & -\frac{308}{3} & 294 & -518 & 287 & -49 & \dots \\ -16 & 104 & -88 & -352 & \frac{1600}{3} & -\frac{592}{3} & 660 & -\frac{3908}{3} & \frac{2476}{3} & -\frac{500}{3} & \dots \\ -18 & 135 & -117 & -546 & 864 & -336 & 1287 & -2733 & 1884 & -420 & \dots \\ -20 & 170 & -150 & -800 & \frac{3920}{3} & -\frac{1580}{3} & 2275 & -5085 & 3715 & -885 & \dots \end{pmatrix}.$$

After some calculation, we see that

$$\begin{aligned} \gamma_{n1} &= -2 - 2(n - 1) = -2n; \\ \gamma_{n2} &= 2 + 7(n - 2) + 2(n - 2)(n - 3); \\ \gamma_{n3} &= 2 - 5(n - 2) - 2(n - 2)(n - 3); \\ \gamma_{n4} &= -2 - 14(n - 3) - 10(n - 3)(n - 4) - \frac{4}{3}(n - 3)(n - 4)(n - 5); \\ \gamma_{n5} &= \frac{1}{3}(32(n - 3) + 48(n - 3)(n - 4) + 8(n - 3)(n - 4)(n - 5)); \\ \gamma_{n6} &= -4 + \frac{4}{3}(n - 3) - 6(n - 3)(n - 4) - \frac{4}{3}(n - 3)(n - 4)(n - 5); \\ \gamma_{n7} &= 2 + 23(n - 4) + 28.5(n - 4)(n - 5) + \frac{26}{3}(n - 4)(n - 5)(n - 6) \\ &\quad + \frac{2}{3}(n - 4)(n - 5)(n - 6)(n - 7); \\ \gamma_{n8} &= 2 - \frac{71}{3}(n - 4) - \frac{317}{6}(n - 4)(n - 5) - 22(n - 4)(n - 5)(n - 6) \\ &\quad - 2(n - 4)(n - 5)(n - 6)(n - 7); \\ \gamma_{n9} &= -6 + \frac{28}{3}(n - 4) + \frac{157}{6}(n - 4)(n - 5) + 18(n - 4)(n - 5)(n - 6) \\ &\quad + 2(n - 4)(n - 5)(n - 6)(n - 7); \\ \gamma_{n10} &= 10 - \frac{20}{3}(n - 4) - \frac{11}{6}(n - 4)(n - 5) - \frac{14}{3}(n - 4)(n - 5)(n - 6) \\ &\quad - \frac{2}{3}(n - 4)(n - 5)(n - 6)(n - 7) \end{aligned}$$

is valid for all n . This implies that we know the entire column of Γ as soon as the first entries are known.

The regularity of the above matrix Γ is expressed in the following theorem.

Theorem 2. *Let $\Gamma = (\gamma_{jk})$ be the matrix defined in (2.9), (2.10), (2.4), (2.5). For each fixed $k = 1, 2, \dots$, there exists a polynomial $\pi_k \in \Pi_{j_0}$ such that*

$$(2.13) \quad \gamma_{jk} = \pi_k(j) \quad \text{for all } j \geq j_0,$$

where j_0 is uniquely defined by

$$(2.14) \quad j_0(j_0 + 1)/2 < k \leq (j_0 + 1)(j_0 + 2)/2.$$

Proof. By the recursion (2.8), using induction. \square

The above γ_{jk} are just the coefficients of the polynomial $p_{j-1, j_0} \in \Pi_{j_0}$. In order to compute the π_k , we interpolate the first entries of column k of Γ . That is, we interpolate the points (j, γ_{jk}) for $j = j_0, j_0 + 1, \dots, 2j_0$. If we choose the Newton form for π_k , then the result can be put in the form

$$(2.15) \quad \begin{aligned} \pi_k(n) &= d_{0k} + d_{1k}(n - j_0) + d_{2k}(n - j_0)(n - j_0 - 1) \\ &\quad + \dots + d_{j_0k}(n - j_0)(n - j_0 - 1) \cdots (n - 2j_0 + 1), \end{aligned}$$

and we can store these results in a matrix

$$(2.16) \quad D = (d_{jk}), \quad k = 1, 2, \dots; \quad j = 0, 1, \dots, j_0,$$

where j_0 was already defined in (2.14). Examples were already given directly after matrix (2.12).

Suppose we know the first n Faber polynomials, or, equivalently, the matrix Γ_n . By Theorem 2, the first $[n/2]([n/2] + 1)/2$ columns of the infinite matrix Γ are known completely. Here, $[x]$ denotes the largest integer less than or equal

to x . In particular, Theorem 2 gives full information about the growth of the coefficients of the Faber polynomials.

3. TWO-NORMS AND INFINITY NORM OF FABER POLYNOMIALS ON CIRCULAR SECTORS

We now consider $\|F_n\|_\infty$ and $\|F_n\|_2$. Note that the latter norm can be explicitly computed. In the case of the two-norm, we will consider the area norm and the line norm separately. We also state a conjecture about the uniform norm that would allow an explicit and easy computation of $\|F_n\|_\infty$.

3.1. The area norm of Faber polynomials on circular sectors. In order to compute the (area) two-norm, assume first that the opening angle α of the sector S_α is positive. In this case, the square of the two-norm of the scaled Faber polynomials (cf. (2.6)) is

$$(3.1) \quad \|\tilde{F}_n\|_2^2 = \int_{S_\alpha} |\Phi_n(z/\rho)|^2 dx dy = \rho^2 \int_{S_\alpha/\rho} |\Phi_n(u)|^2 dv dw,$$

where $z = x + iy$, $u = v + iw$, and S_α/ρ is the sector with radius $1/\rho$ and opening angle 2α . Using (2.5') and (2.7), we have

$$(3.2) \quad \begin{aligned} |\Phi_n(u)|^2 &= |u^n + (1 - c)\phi_{n-1}(u)|^2 \\ &= |u|^{2n} + 2(1 - c)\Re\{\bar{u}^n \phi_{n-1}(u)\} + (1 - c)^2 |\phi_{n-1}(u)|^2, \end{aligned}$$

where the overbar denotes complex conjugation and \Re denotes the real part of the corresponding complex number. Thus, the problem is reduced to integrating terms of the form $\Re u^s \bar{u}^t$, $s, t \geq 0$. Using polar coordinates, we obtain

$$(3.3) \quad I_{s,t} = \rho^2 \int_{S_\alpha/\rho} \Re u^s \bar{u}^t dv dw = \begin{cases} \frac{2\rho^{-s-t} \sin(s-t)\alpha}{(s-t)(s+t+2)} & \text{for } s \neq t, \\ \frac{\rho^{-2s}\alpha}{s+1} & \text{for } s = t. \end{cases}$$

Combining these results, we obtain for $\alpha > 0$ the following final formula:

$$(3.4) \quad \begin{aligned} \|\tilde{F}_n\|_2^2 &= I_{n,n} + 2(1 - c) \sum_{j=0}^{n-1} p_{n-1,j} I_{n-1-j,n} \\ &+ (1 - c)^2 \sum_{j=0}^{n-1} p_{n-1,j}^2 I_{n-1-j,n-1-j} \\ &+ 2(1 - c)^2 \sum_{j>k}^{n-1} p_{n-1,j} p_{n-1,k} I_{n-1-j,n-1-k}. \end{aligned}$$

In the disk case ($\alpha = \pi$, $c = \rho = 1$), this formula reduces to

$$(3.5) \quad \|\tilde{F}_n\|_2^2 = \|F_n\|_2^2 = \frac{\pi}{n+1}.$$

In the interval case ($\alpha = c = 0$, $\rho = \frac{1}{4}$) we can use the explicit form of the F_n given at the end of §1. The square of the two-norm of the scaled Faber polynomials is then

$$(3.6) \quad \|\tilde{F}_n\|_2^2 = 4 \int_0^1 \cos^2\{n \arccos(2x - 1)\} dx = 2 - \frac{2}{4n^2 - 1}.$$

3.2. The line norm of Faber polynomials on circular sectors. The square of the line norm of the scaled Faber polynomials is defined by

$$(3.7) \quad \|\tilde{F}_n\|_2^2 = \int_{\partial S_\alpha} |\Phi_n(z/\rho)|^2 ds = \rho \int_{\partial S_\alpha/\rho} |\Phi_n(u)|^2 d\sigma,$$

where s is the line element in the z -plane, σ is the line element in the u -plane, and ∂S is the boundary of S . With these conventions, the results of the previous subsection apply essentially unchanged, after replacing the area integrals $I_{s,t}$ given in (3.3) with the corresponding line integrals. For $0 < \alpha < \pi$ these integrals are

$$(3.8a) \quad \hat{I}_{s,t} = \rho \int_{\partial S_\alpha/\rho} \Re u^s \bar{u}^t d\sigma = \begin{cases} 2\rho^{-s-t} \left\{ \frac{\cos(s-t)\alpha}{(s+t+1)} + \frac{\sin(s-t)\alpha}{s-t} \right\} & \text{for } s \neq t, \\ 2\rho^{-2s} \left\{ \frac{1}{2s+1} + \alpha \right\} & \text{for } s = t. \end{cases}$$

For $\alpha = 0$ we delete the factor 2, and for $\alpha = \pi$ we omit the integrals over the straight parts of the sector. So, we obtain

$$(3.8b) \quad \hat{I}_{s,t} = \begin{cases} 4^{s+t}/(s+t+1) & \text{for } \alpha = 0, \\ \begin{cases} 0 & \text{for } s \neq t, \\ 2\pi & \text{for } s = t, \end{cases} & \text{for } \alpha = \pi. \end{cases}$$

Thus, the final formula for $\|\tilde{F}_n\|_2^2$ is the same as formula (3.4), when replacing $I_{s,t}$ with $\hat{I}_{s,t}$ from (3.8a) and (3.8b).

3.3. Infinity norm of Faber polynomials on circular sectors. The results of Coleman and Smith [1], partly due to Pommerenke [10] and Walsh [12, p. 319] are:

$$(3.9) \quad \|T_n\|_\infty \leq \|F_n\|_\infty \leq 2\|T_n\|_\infty,$$

$$(3.10) \quad 1 \leq \|\tilde{F}_n\|_\infty \leq 2,$$

$$(3.11) \quad \lim_{n \rightarrow \infty} \|\tilde{F}_n\|_\infty = \begin{cases} 1 & \text{for } \alpha = \pi, \\ 2(1 - \alpha/\pi) & \text{for } 0 \leq \alpha \leq \pi/4, \end{cases}$$

where \tilde{F}_n are the scaled Faber polynomials as introduced in (2.6).

The situation for obtaining explicit expressions for $\|F_n\|_\infty$ is not so favorable. However, supported by numerical experiments, we formulate the following conjecture.

Conjecture. Assume that $0 < \alpha < \pi$ and $n > 0$. Then the norm $\|F_n\|_\infty$ is always attained at the origin $z = 0$ or at the two corners $z = e^{\pm i\alpha}$ of the sector S_α . For fixed n there is a critical angle α_n such that for $\alpha < \alpha_n$ the norm is attained only at the origin, and for $\alpha > \alpha_n$ the norm is attained only at the two corners. For $\alpha = \alpha_n$ the norm is attained only at the origin and at the two corners.

For $n = 1$ we can find the above critical angle by solving $|F_1(0)| = F_1(e^{i\alpha})|$ for α with a pocket calculator (HP 15C) and obtain as solution $\alpha_1 \approx 0.61838434$

TABLE 1
Critical angles for Faber polynomials F_n on sectors

n	alpha(deg)	alpha
1	35.430813	0.61838434
2	59.059789	1.03078777
3	43.672788	0.76223395
4	46.840804	0.81752625
5	44.221977	0.77181909
6	47.007470	0.82043512
7	45.619633	0.79621279
8	43.976473	0.76753425
9	45.575804	0.79544783
10	45.511724	0.79432944
11	45.399940	0.79237843
12	44.403878	0.77499388
13	45.732598	0.79818441
14	45.099206	0.78712963
15	45.112012	0.78735314
16	44.837307	0.78255863
17	45.535540	0.79474510
18	45.097395	0.78709802
19	44.829223	0.78241755
20	45.129013	0.78764986

$\approx 35.430813^\circ$. According to our numerical tests, the critical angles for $3 \leq n \leq 20$ are all close to, but not equal to, $\pi/4$. For $n = 2$, the critical angle is approximately 60° . The computed values are shown in Table 1.

In geometric terms, the above conjecture means that the *contour line* (or *lemniscate*) $L = \{z \in \mathbb{C} : |F_n(z)| = \|F_n\|_\infty\}$ contains the underlying sector S_α in its interior and touches it at most at the corners of the sector. A graph for $\alpha = \pi/4$, $n = 4$ is given in Figure 1. It was produced with MATLAB from data computed by a Pascal program. Generally, these contour lines approach the sector S_α with increasing degree n . A similar graph for a Chebyshev polynomial is given by Grothkopf and Opfer [8]. Some selected values of $\|\tilde{F}_{10}\|$ for all considered norms are shown in Table 2.

An upper bound for the two-norms is easily obtained by means of infinity norms. If p_n is any polynomial in Π_n on the sector S_α , we have for $\alpha > 0$

$$(3.12) \quad \|p_n\|_2 \leq \sqrt{\alpha} \|p_n\|_\infty, \quad \hat{\|p_n\|}_2 \leq \hat{c} \|p_n\|_\infty,$$

$$\hat{c} = \begin{cases} \sqrt{2 + 2\alpha} & \text{for } 0 < \alpha < \pi, \\ \sqrt{2\pi} & \text{for } \alpha = \pi. \end{cases}$$

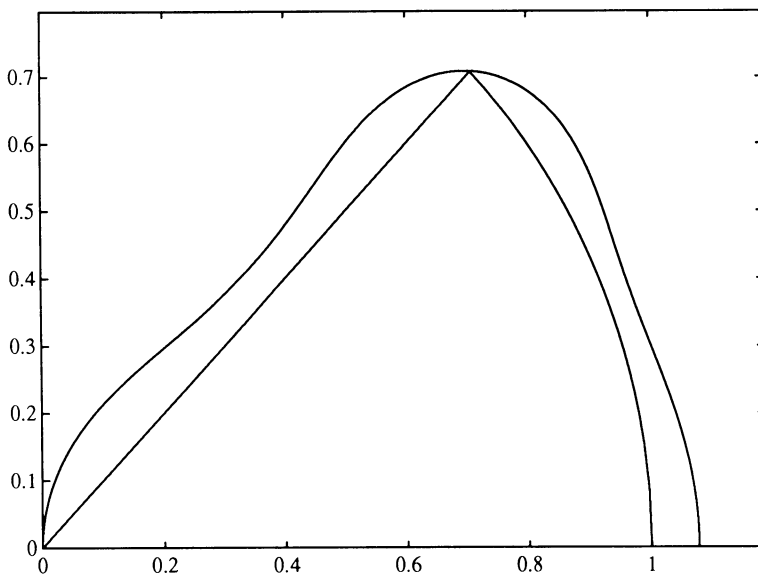


FIGURE 1
 Lemniscate of Faber polynomial F_4 on quarter disk (upper half)

TABLE 2
 Norms of \tilde{F}_{10} for selected opening angles

Angle(deg)	Area norm	Line norm	Max norm
0	1.41244	1.41244	2.00000
1	0.14464	1.73706	1.99486
2	0.17507	1.63409	1.98289
5	0.20528	1.54936	1.93763
10	0.22675	1.56115	1.88580
15	0.24195	1.60252	1.84438
30	0.28744	1.75067	1.65220
45	0.33064	1.89025	1.51534
60	0.37649	2.02449	1.49257
90	0.47260	2.26905	1.49433
120	0.62861	2.48243	1.47365
135	0.72261	2.57852	1.38143
150	0.71351	2.60358	1.68426
165	0.55964	2.52959	1.68443
170	0.53384	2.51431	1.43410
175	0.52961	2.51008	1.14367
178	0.53194	2.51550	1.02539
179	0.53307	2.51966	1.00645
180	0.53441	2.50663	1.00000

4. REPORT ON COMPUTATIONS

We used several computers and symbolic algebra systems, as listed in Table 3. The SIEMENS 7.882 computer is a large mainframe, the Symbolics 3650 is a workstation whose native language is Lisp, and the other computers are personal microcomputers.

We tested our algorithms on the various machines by computing the Faber polynomials up to a certain degree n and observing the corresponding computing times. Denote by time_n the computing time for computing all Faber polynomials up to degree n for a fixed combination of computer and program. We observed in our experiments that the quotient $q_n = \text{time}_n / \text{time}_{n-1}$ depended on the specific computer and program, but was almost independent of n . Thus, the computing time can be predicted by the formula

$$(4.1) \quad \text{time}_n = (q_{n_0})^{n-n_0} \text{time}_{n_0}, \quad n \geq n_0.$$

Table 4 summarizes our observations.

TABLE 3
List of computers and languages used

Case No.	Computer	Language
I	SIEMENS 7.882	REDUCE 3.3 ©Rand Corporation
II	IBM PS/2 Modell 70 A21	REDUCE 3.3 ©Northwest Computer Algorithms
III	Symbolics 3650	MACSYMA 414.62 ©Symbolics
IV	IBM PS/2 Modell 70 A21	MATHEMATICA ©1988 Wolfram Research
V	ATARI MEGA ST4	RIEMANN 1.b ©1989 Jörg Begemann und Alexander Niemeyer

TABLE 4
Behavior of computer/programsystem with respect to algorithm

	I	II	III	IV	V
time for $n = 10$	2.7' †	†	19''	9'25''	9'49''
last n	20	9	20	15	20
time for last n	18.0'	1.5' ‡	7.4'	22h50'	10h58'
$\text{time}_n / \text{time}_{n-1}$	1.22	1.50	1.63	2.69	1.46

† Not available because of memory overflow.

‡ Most likely wrongly reported by REDUCE.

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Supplement to
**EXPLICIT FABER POLYNOMIALS
ON CIRCULAR SECTORS**

KARIN GATERMANN, CHRISTOPH HOFFMANN, AND GERHARD OFFER

Appendix

Table 5. Faber polynomials up to degree 20

Polynomials $\phi_{n-1} = \sum_{j=0}^{n-1} p_j z^{n-j-1}$ for $1 \leq n \leq 20$,
cf. (2.7), (2.9)

1	Degree of Faber polynomial:	1
2	$p(0)$:	-2
3		
4	Degree of Faber polynomial:	2
5	$p(0)$:	-4
6	$p(1)$:	$2 + 2C$
7		
8	Degree of Faber polynomial:	3
9	$p(0)$:	-6
10	$p(1)$:	$9 - 3C$
11	$p(2)$:	$-2 - 4C^2$
12		
13	Degree of Faber polynomial:	4
14	$p(0)$:	-8
15	$p(1)$:	$20 - 12C$
16	$p(2)$:	$-16 + 32/3C - 8/3C^2$
17	$p(3)$:	$2 + 2C - 6C^2 + 10C^3$
18		
19	Degree of Faber polynomial:	5
20	$p(0)$:	-10
21	$p(1)$:	$35 - 25C$
22	$p(2)$:	$-50 + 160/3C - 40/3C^2$
23	$p(3)$:	$25 - 65/3C + 10/3C^2 + 10/3C^3$
24	$p(4)$:	$-2 - 12C^2 + 32C^3 - 28C^4$
25		
26	Degree of Faber polynomial:	6
27	$p(0)$:	-12
28	$p(1)$:	$54 - 42C$
29	$p(2)$:	$-112 + 144C - 44C^2$
30	$p(3)$:	$105 - 151C + 65C^2 - 7C^3$
31	$p(4)$:	$-36 + 192/5C - 16C^2 + 64/5C^3 - 56/5C^4$
32	$p(5)$:	$2 + 2C - 16C^2 + 80C^3 - 140C^4 + 84C^5$
33		

- 34 Degree of Faber polynomial: 7
 35 p(0): -14
 36 p(1): 77 - 63 C
 37 p(2): -210 + 896/3 C - 308/3 C²
 38 p(3): -210 + 896/3 C - 308/3 C²
 39 p(4): -198 + 5152/15 C - 616/3 C² + 784/15 C³ - 42/5 C⁴
 40 p(5): 49 - 889/15 C + 847/45 C² + 119/5 C³ - 161/3 C⁴ + 1589/45 C⁵
 41 p(6): -2 + 24 C² + 160 C³ - 460 C⁴ + 576 C⁵ - 284 C⁶
 42
 43 Degree of Faber polynomial: 8
 44 p(0): -16
 45 p(1): 104 - 88 C
 46 p(2): -352 + 1800/3 C - 592/3 C²
 47 p(3): 660 - 3808/3 C + 2476/3 C² - 500/3 C³
 48 p(4): -672 + 7296/5 C - 1120 C² + 1792/5 C³ - 208/5 C⁴
 49 p(5): 336 - 10192/15 C + 22336/45 C² - 768/5 C³ + 8/3 C⁴ + 632/45 C⁵
 50 p(6): -64 + 9088/105 C - 14752/315 C² + 19456/315 C³ - 18112/105 C⁴ + 73792/315 C⁵
 51 p(7): -36304/315 C⁶
 52 p(8): 2 + 2 C - 30 C² + 280 C³ - 1180 C⁴ + 2394 C⁵ - 2310 C⁶ + 858 C⁷
 53
 54 Degree of Faber polynomial: 9
 55 p(0): -18
 56 p(1): 135 - 117 C
 57 p(2): -546 + 864 C - 336 C²
 58 p(3): 1287 - 2733 C + 1884 C² - 420 C³
 59 p(4): -1782 + 21888/5 C - 3876 C² + 7296/5 C³ - 984/5 C⁴
 60 p(5): 1386 - 17538/5 C + 18713/5 C² - 7431/5 C³ + 300 C⁴ - 84/5 C⁵
 61 p(6): -540 + 8544/7 C - 36536/35 C² + 16536/35 C³ - 5322/35 C⁴ + 736/7 C⁵
 62 p(7): -1808/35 C⁶
 63 p(8): 81 - 4149/35 C + 369/7 C² + 2837/35 C³ - 15089/35 C⁴ + 945 C⁵ - 4886/5 C⁶
 64 p(9): 13478/35 C⁷
 65 p(10): -2 - 40 C² + 480 C³ - 2580 C⁴ + 7616 C⁵ - 11704 C⁶ + 9152 C⁷ - 2860 C⁸
 66
 67 Degree of Faber polynomial: 10
 68 p(0): -20
 69 p(1): 170 - 150 C
 70 p(2): -800 + 3920/3 C - 1580/3 C²
 71 p(3): 2275 - 5085 C + 3715 C² - 885 C³
 72 p(4): -4004 + 32000/3 C - 31072/3 C² + 12992/3 C³ - 656 C⁴
 73 p(5): 4290 - 12382 C + 123488/9 C² - 7264 C³ + 5480/3 C⁴ - 1544/9 C⁵
 74 p(6): -2640 + 52688/7 C - 58908/7 C² + 32896/7 C³ - 9760/7 C⁴ + 1654/7 C⁵
 75 p(7): -240/7 C⁶
 76 p(8): 825 - 42856/21 C + 123391/63 C² - 57385/63 C³ + 594/7 C⁴ + 3086/9 C⁵
 77 p(9): -3746/9 C⁶ + 3668/21 C⁷
 78 p(10): -100 + 9920/63 C - 6352/63 C² + 101440/567 C³ - 78808/81 C⁴ + 1660872/587 C⁵
 79 p(11): -38920/81 C⁶ + 2261696/567 C⁷ - 743464/567 C⁸
 80 p(12): 2 + 2 C - 46 C² + 752 C³ - 5346 C⁴ + 20412 C⁵ - 44352 C⁶ + 54912 C⁷
- 81 - 36036 C⁸ + 9724 C⁹
 82 Degree of Faber polynomial: 11
 83 p(0): -22
 84 p(1): 209 - 187 C
 85 p(2): -1122 + 5652/3 C - 2332/3 C²
 86 p(3): 3740 - 26046/3 C + 18656/3 C² - 4961/3 C³
 87 p(4): -8008 + 12892/5 C - 39408 C² + 52624/5 C³ - 8646/5 C⁴
 88 p(5): 11011 - 104071/3 C + 381887/9 C² - 25113 C³ + 21508/3 C⁴ - 7073/9 C⁵
 89 p(6): -9438 + 1081344/35 C - 12729904/315 C² + 1696640/63 C³ - 336424/35 C⁴
 90 p(7): 4719 - 518639/35 C + 656722/35 C² - 432014/35 C³ + 157014/35 C⁴ - 3894/5 C⁵
 91 p(8): -418/5 C⁶ + 2706/35 C⁷
 92 p(9): -1210 + 203104/63 C - 153736/45 C² + 5418688/2835 C³ - 2565992/2835 C⁴
 93 p(10): 3489376/2835 C⁵ - 811888/405 C⁶ + 996160/567 C⁷ - 17256988/2835 C⁸
 94 p(11): 121 - 63481/315 C + 19294/175 C² + 2870846/14175 C³ - 12525504/675 C⁴
 95 p(12): 7245128/945 C⁵ - 50424044/2835 C⁶ + 110129632/4725 C⁷ - 75894702/4725 C⁸
 96 p(13): 64269864/14175 C⁹
 97 p(14): -2 - 60 C² + 1120 C³ - 9940 C⁴ + 46384 C⁵ - 139104 C⁶ + 242112 C⁷
 98 p(15): -250360 C⁸ + 141440 C⁹ - 33592 C¹⁰
 99
 100 Degree of Faber polynomial: 12
 101 p(0): -24
 102 p(1): 252 - 228 C
 103 p(2): -1520 + 2692 C - 1086 C²
 104 p(3): 5814 - 13896 C + 10942 C² - 2834 C³
 105 p(4): -14688 + 216394/5 C - 47024 C² + 111488/5 C³ - 19432/5 C⁴
 106 p(5): 24752 - 415248/5 C + 544768/5 C² - 348576/5 C³ + 21708 C⁴ - 13124/5 C⁵
 107 p(6): -27456 + 690560/7 C - 3007264/21 C² + 2251264/21 C³ - 304704/7 C⁴
 108 p(7): 190432/21 C⁵ - 15928/21 C⁶
 109 p(8): 19305 - 49001/7 C + 3649147/35 C² - 8649679/105 C³ + 779909/21 C⁴
 110 p(9): -47371/5 C⁵ + 18079/15 C⁶ - 3519/105 C⁷
 111 p(10): -8008 + 40852/15 C - 4009192/105 C² + 1002486/35 C³ - 1325152/105 C⁴
 112 p(11): 1716 - 511564/105 C + 139648/25 C² - 15603712/4725 C³ + 837296/1575 C⁴
 113 p(12): 831728/315 C⁵ - 15691856/1575 C⁶ + 15691856/1575 C⁷ - 11394616/1575 C⁸
 114 p(13): 10093592/4725 C⁹
 115 p(14): -144 + 87376/385 C - 1055848/5775 C² + 636928/1575 C³ - 35404872/10395 C⁴
 116 p(15): 308338816/17325 C⁵ - 188927392/3465 C⁶ + 5214330112/51975 C⁷
 117 p(16): 1887787168/17325 C⁸ + 24754496/385 C⁹ - 62532528/51975 C¹⁰
 118 p(17): 2 + 2 C - 70 C² + 1610 C³ - 17360 C⁴ + 104496 C⁵ - 380688 C⁶ + 871728 C⁷
 119 p(18): -1261260 C⁸ + 1118260 C⁹ - 554268 C¹⁰ + 117572 C¹¹
 120
 121 Degree of Faber polynomial: 13
 122 p(0): -26
 123 p(1): 289 - 273 C
 124 p(2): -2002 + 10400/3 C - 44772/3 C²

- 128 p(3): 8645 - 21151 C + 17082 C² - 4550 C³
 129 p(4): -25194 + 1161468/15 C - 286963/3 C² + 641056/15 C³ - 38948/5 C⁴
 130 p(5): 50388 - 2659592/16 C + 11030463/45 C² - 830843/5 C³ + 55146 C⁴ - 321988/45 C⁵
 131 p(6): -68952 + 9277216/35 C - 14510288/35 C² + 11796304/35 C³ - 52404254/35 C⁴
 132 + 1207648/35 C⁵ - 112216/35 C⁶
 133 p(7): 63206 - 5308062/21 C + 26442286/63 C² - 23572978/63 C³ + 4050878/21 C⁴
 134 - 516022/9 C⁵ + 81445/9 C⁶ - 11989/21 C⁷
 135 p(8): -37180 + 9251840/63 C - 76579984/315 C² + 622514048/2835 C³ - 334511944/2835 C⁴
 136 + 16546592/405 C⁵ - 3147504/405 C⁶ + 3174496/2835 C⁷ - 13702/81 C⁸
 137 p(9): 13013 - 711581/15 C + 31927103/525 C² - 31625113/525 C³ + 2241421/75 C⁴
 138 - 864721/105 C⁵ - 116701/105 C⁶ + 101807/25 C⁷ - 572169/175 C⁸ + 177931/175 C⁹
 139 p(10): -23666 + 3513536/495 C - 16797456/1925 C² + 82967872/14175 C³ - 5039944/1485 C⁴
 140 + 38816958/15175 C⁵ - 8704728/31185 C⁶ + 11480768/275 C⁷
 141 - 2479880764/51975 C⁸ + 918234304/31185 C⁹ - 56225104/7425 C¹⁰
 142 p(11): -1073579/3465 C + 1456110/7425 C² + 60056876/15825 C³ - 2723192888/467775 C⁴
 143 + 2520148904/66825 C⁵ - 3255665156/22275 C⁶ + 15027228292/42525 C⁷
 144 - 22815606038/42525 C⁸ + 23465687002/4725 C⁹ - 10851233428/42525 C¹⁰
 145 + 3756520508/66825 C¹¹
 146 p(12): -2 - 84 C² + 2240 C³ - 28840 C⁴ + 209684 C⁵ - 938784 C⁶ + 2709696 C⁷
 147 - 5134140 C⁸ + 6343040 C⁹ - 4917352 C¹⁰ + 2170560 C¹¹ - 416024 C¹²
 148 Degree of Faber polynomial: 14
 149 p(0): -28
 150 p(1): 350 - 322 C
 151 p(2): -2576 + 13562/3 C - 5908/3 C²
 152 p(3): 12397 - 92759/3 C + 76447/3 C² - 20825/3 C³
 153 p(4): -40964 + 641088/5 C - 148948 C² + 379456/5 C³ - 71624/5 C⁴
 154 p(5): 94892 - 1734278/5 C + 22475152/45 C² - 1769936/5 C³ + 123340 C⁴ - 769556/45 C⁵
 155 p(6): -185640 + 1682384/3 C - 46720132/45 C² + 4038672/45 C³ - 6406928/15 C⁴
 156 p(7): 952736/9 C⁵ - 479656/45 C⁶
 157 + 219219/5 C⁶ - 16061/5 C⁷
 158 p(8): -136136 + 5358360/9 C - 3310304/3 C² + 91418432/81 C³ - 56314960/81 C⁴
 159 + 21345728/81 C⁵ - 4868448/81 C⁶ + 614464/81 C⁷ - 36500/81 C⁸
 160 p(9): 68088 - 13015008/45 C + 117695968/225 C² - 1066942432/2025 C³ + 219139976/675 C⁴
 161 - 17037784/135 C⁵ + 12140032/405 C⁶ - 1892384/675 C⁷ - 754426/675 C⁸
 162 + 963602/2025 C⁹
 163 p(10): -20384 + 13013728/165 C - 106354312/625 C² + 8825984/75 C³ - 726048/11 C⁴
 164 + 21246948/625 C⁵ - 2273168/165 C⁶ + 15014272/825 C⁷ - 5789088/275 C⁸
 165 + 149392/11 C⁹ - 1001756/275 C¹⁰
 166 p(11): 3185 - 927845/99 C + 19410837/1485 C² - 202989581/22275 C³ + 133028931/68825 C⁴
 167 - 189167037/6075 C⁵ - 124676515/22275 C⁶ + 174414133/1215 C⁷
 168 + 1609576513/66825 C⁸ - 149636831/675 C⁹ - 144435683/1215 C¹⁰
 169 p(12): -196 + 2409344/6435 C + 5874734848/78975 C² + 227724416/286575 C³
 170 - 8317421392/668735 C⁴ + 5874734848/78975 C⁵ - 23635109538/66825 C⁶
 171 + 187048177216/173745 C⁷ - 168902447048/78975 C⁸ + 217728307072/78975 C⁹
 172 - 175391052888/78975 C¹⁰ + 881790850528/668735 C¹¹ - 174467231152/668735 C¹²
 173 + 17889300 C¹³ + 28831660 C⁹ - 31039008 C¹⁰ + 21364512 C¹¹ - 8488776 C¹²
 174 - 1465800 C¹³
 175 Degree of Faber polynomial: 15
 176 p(0): -30
 177 p(1): 405 - 375 C
 178 p(2): -3250 + 5760 C - 2540 C²
 179 p(3): 17250 - 43680 C + 36635 C² - 10165 C³
 180 p(4): -63756 + 204000 C - 242638 C² + 126896 C³ - 24634 C⁴
 181 p(5): 168245 - 632283 C + 942083 C² - 691741 C³ + 250465 C⁴ - 35739 C⁵
 182 p(6): -319770 + 9434112/7 C - 48939656/21 C² + 44391392/21 C³ - 7416880/7 C⁴
 183 + 5835988/21 C⁵ - 624920/21 C⁶
 184 p(7): 436050 - 1976850 C + 3727303 C² - 11738075/3 C³ + 7141039/3 C⁴ - 868098 C⁵
 185 + 480777/3 C⁶ - 39463/3 C⁷
 186 p(8): -415900 + 4157600/7 C - 6327536/21 C² + 3118760/7 C³ - 63556012/210 C⁴
 187 + 28796064/21 C⁵ - 325480 C⁶ + 321184/7 C⁷ - 19267/7 C⁸
 188 p(9): 277134 - 27485938/21 C + 5683650/21 C² - 57510204/189 C³ + 135874552/63 C⁴
 189 - 61708384/63 C⁵ + 53684602/189 C⁶ - 3152482/63 C⁷ + 275485/63 C⁸ + 4465/189 C⁹
 190 p(10): -118340 + 41601792/7 C - 1217323432/1155 C² + 17448832/15 C³ - 238264984/297 C⁴
 191 + 1250696704/3465 C⁵ - 75856304/693 C⁶ + 287039968/10395 C⁷ - 40449022/3465 C⁸
 192 + 4475456/693 C⁹ - 18410012/10395 C¹⁰
 193 p(11): 30940 - 4163116/33 C + 254226878/1155 C² - 83171342/385 C³ + 30371276/231 C⁴
 194 - 55193492/1155 C⁵ - 687432/77 C⁶ + 5876312/105 C⁷ - 10271524/105 C⁸
 195 + 99384 C⁹ - 277813/5 C¹⁰ + 1011891/77 C¹¹
 196 p(12): -4200 + 5022880/429 C - 24419888/1287 C² + 1964038432/135135 C³
 197 - 3954095536/405405 C⁴ + 11470992928/405405 C⁵ - 4166569248/31185 C⁶
 198 + 17357234176/405405 C⁷ - 4700841688/5265 C⁸ + 44312401856/38855 C⁹
 199 - 3713357048/38855 C¹⁰ + 19350580304/405405 C¹¹ - 39558110386/405405 C¹²
 200 p(13): 225 - 445256/1001 C + 698673/21021 C² + 27607303/35035 C³ + 14183210761/945945 C⁴
 201 + 3927901847/283785 C⁵ - 223959699403/283785 C⁶ + 116951642859/405405 C⁷
 202 - 465869752716/237 C⁸ + 24376621921/19945 C⁹ - 272515606979/19945 C¹⁰
 203 + 2136340048511/218295 C¹¹ - 877129512661/218295 C¹² + 205223586867/283785 C¹³
 204 p(14): -2 - 112 C² + 4032 C³ - 70728 C⁴ + 712320 C⁵ - 4520208 C⁶ + 19081920 C⁷
 205 - 55274076 C⁸ + 111398144 C⁹ - 155934064 C¹⁰ + 148611008 C¹¹ - 91941304 C¹²
 206 + 33281920 C¹³ - 5348880 C¹⁴
 207 Degree of Faber polynomial: 16
 208 p(0): -32
 209 p(1): 464 - 432 C
 210 p(2): -4032 + 21632/3 C - 9632/3 C²
 211 p(3): 23400 - 60056 C + 51080 C² - 14392 C³
 212 p(4): 85680 + 487376/15 C - 113400/3 C² + 3031552/15 C³ - 200736/5 C⁴
 213 p(5): 263360 - 3279667/3 C + 16033728/9 C² - 1262336 C³ + 1414480/3 C⁴ - 626192/9 C⁵
 214 p(6): -615296 + 93798144/35 C - 160848576/35 C² + 31676416/7 C³ - 82742144/35 C⁴
 215 + 22695652/35 C⁵ - 2550816/35 C⁶

- 222 p(7): 980828 - 162608004/35 C + 2925611228/315 C² - 3192440996/315 C³ + 663987012/105 C⁴
- 223 - 110648560/45 C⁵ + 228046028/45 C⁶ - 1529394/35 C⁷
- 224 p(8): -1136529 + 51118552/9 C - 182448792/16 C² + 5896589184/405 C³ - 4513406016/405 C⁴
- 225 + 196661788/405 C⁵ - 547637888/405 C⁶ + 16928768/81 C⁷ - 5663424/405 C⁸
- 226 p(9): 940576 - 72048928/15 C + 5577828352/525 C² - 7002189312/525 C³ + 5485991648/525 C⁴
- 227 - 565096928/105 C⁵ + 265944416/15 C⁶ - 8776832/25 C⁷ + 6967344/175 C⁸
- 228 - 46128/25 C⁹
- 229 p(10): -537472 + 1880406784/893 C - 4133141440/893 C² + 4262636832/567 C³
- 230 - 12396843520/2079 C⁴ + 928237312/297 C⁵ - 6813285568/4237 C⁶ + 526283776/2079 C⁷
- 231 - 3279320/2079 C⁸ + 36540800/6237 C⁹ - 31840/33 C¹⁰
- 232 p(11): 201552 - 1114434094/1155 C + 10448002512/51975 C² - 24940156472/10395 C³
- 233 + 860276314698/487775 C⁴ - 42757784232/467775 C⁵ + 47401039652/15925 C⁶
- 234 - 2047380828/42625 C⁷ - 2649826356/8505 C⁸ + 619344424/14175 C⁹
- 235 - 1017809088/42625 C¹⁰ + 3003589104/467775 C¹¹
- 236 p(12): -46698 + 13676832/715 C + 27202706848/76076 C² + 9443912704/26025 C³
- 237 - 188216607488/76076 C⁴ + 2973872128/26025 C⁵ - 477526828/576 C⁶
- 238 + 13278940832/76076 C⁷ + 5645832832/8825 C⁸ + 3689350888/6825 C⁹
- 239 - 1044160448/2275 C¹⁰ + 26549540288/25025 C¹¹ - 170579424/3575 C¹²
- 240 p(13): 5440 - 167444672/9009 C + 25297177856/946945 C² - 289232786496/14189175 C³
- 241 + 2178974896/386975 C⁴ + 1909844215904/42567525 C⁵ - 12393554484736/42567525 C⁶
- 242 - 198799846912/173745 C⁷ - 1398354847168/467775 C⁸ + 1561081208128/297675 C⁹
- 243 - 1814895116288/297675 C¹⁰ + 1473828993792/3274425 C¹¹ - 1250176091782/664885 C¹²
- 244 + 558079309328/1676575 C¹³
- 245 p(14): -256 + 235685824/45045 C - 2116343168/4729725 C² + 97978413056/70946875 C³
- 246 - 4870103181056/12387625 C⁴ + 22374877345024/91216125 C⁵
- 247 - 67446436743956/30406375 C⁶ + 1730209082619982/23648625 C⁷
- 248 - 8093148641584/30406375 C⁸ + 76273501700864/16372125 C⁹
- 249 - 3732144603776/55125 C¹⁰ + 1214465573681624/1819125 C¹¹ + 14243039912704/334125 C¹²
- 250 + 68993787104896/4343625 C¹³ - 167418048651168/638612876 C¹⁴
- 251 p(15): 2 + 2 C - 126 C² + 5260 C³ - 105630 C⁴ + 1227618 C⁵ - 9069568 C⁶ + 44936034 C⁷
- 252 - 155070630 C⁸ + 379409170 C⁹ - 662073126 C¹⁰ + 181824762 C¹¹ - 699034326 C¹²
- 253 + 392822850 C¹³ - 130378950 C¹⁴ + 18389990 C¹⁵
- 254 Degree of Faber polynomial: 17
- 255 p(0): -34
- 256 p(1): 427 - 493 C
- 257 p(2): -5830 + 28654/3 C - 11988/3 C²
- 258 p(3): 31059 - 241859/3 C + 208216/3 C² - 59432/3 C³
- 259 p(4): -139230 + 3204384/5 C - 568278 C² + 1546048/5 C³ - 313072/5 C⁴
- 260 p(5): 487470 - 27032074/15 C + 126088777/45 C² - 10894671/5 C³ + 2504984/3 C⁴
- 261 - 569989/45 C⁵
- 262 p(6): -1118260 + 10513520/21 C - 581638952/63 C² + 566658784/63 C³ - 101876934/21 C⁴
- 263 + 86928304/63 C⁵ - 10158666/63 C⁶
- 264 p(7): 2042975 - 70215987/7 C + 728799027/35 C² - 828458093/35 C³ + 111289429/7 C⁴
- 265 - 31517641/5 C⁵ + 6623188/5 C⁶ - 4350708/35 C⁷
- 266 p(8): -21778446 + 457828692/315 C - 10302837896/315 C² + 117123982816/2835 C³
- 267 - 1937620 + 310536350/35 C - 587009646/35 C² + 865976424/35 C³ - 325896904/35 C⁴
- 268 - 12360610892/405 C⁴ + 8815758272/567 C⁵ - 1871729512/405 C⁶ + 2175721472/2835 C⁷
- 269 - 154353064/2835 C⁸
- 270 p(9): 2778446 - 873904318/45 C + 8008239317/225 C² - 97094496643/2025 C³
- 271 + 27376353696/875 C⁴ - 3011517343/135 C⁵ + 3226572613/405 C⁶
- 272 - 1200891181/875 C⁷ + 151796876/675 C⁸ - 24728812/2025 C⁹
- 273 p(10): -1989724 + 18053154692/165 C - 154267446828/5775 C² + 19064871136/525 C³
- 274 - 11321876896/575 C⁴ + 10828144445/5775 C⁵ - 1706424360/231 C⁶ - 3169344/1825 C¹⁰
- 275 + 112767622/1925 C⁷ - 6165764522/1925 C⁸ + 12065376/385 C⁹ - 3169344/1825 C¹⁰
- 276 p(11): 999362 - 529717588/99 C + 261887222404/2079 C² - 153005164289/991 C³
- 277 + 2813444865844/18711 C⁴ - 16578383576/18711 C⁵ + 2477960214/693 C⁶
- 278 - 166567578/18711 C⁷ + 280312815/1701 C⁸ - 753355/587 C⁹ - 2643160/243 C¹⁰
- 279 + 58303880/18711 C¹¹
- 280 p(12): -328460 + 4977761024/3003 C - 494521734328/135135 C² + 315916230688/676575 C³
- 281 - 424691735464/110665 C⁴ + 12984175488512/6081075 C⁵ - 391483435936/487775 C⁶
- 282 + 1736489329184/6081075 C⁷ - 108501120722/562825 C⁸ + 26024819648/110665 C⁹
- 283 - 116192020172/562825 C¹⁰ + 651812715988/6081075 C¹¹ - 142737082864/6081075 C¹²
- 284 p(13): 65892 - 1469083828/5005 C + 99571631634/176175 C² - 30161589278/47775 C³
- 285 + 234323153164/525625 C⁴ - 10315943972/525625 C⁵ - 3971613304/105105 C⁶
- 286 + 10758534194/25025 C⁷ - 840778904/525 C⁸ + 2746486744/1225 C⁹
- 287 - 9971703821/5675 C¹⁰ + 5899413189/2686 C¹¹ - 12276267544/13475 C¹²
- 288 + 2774882744/15825 C¹³
- 289 p(14): -6936 + 368480576/16015 C - 174213995652/4729725 C² + 2219173813088/70946875 C³
- 290 - 5006450476348/12837625 C⁴ + 8192218813152/91216125 C⁵
- 291 - 18265738511792/30406375 C⁶ + 45897548634688/16372125 C⁷
- 292 - 270711825836088/30406375 C⁸ + 3193242899058472/16372125 C⁹
- 293 - 43837950549296/1488375 C¹⁰ + 49256488057008/16372125 C¹¹
- 294 - 46393247892434/2338875 C¹² + 771465397415072/10135125 C¹³
- 295 - 824775229682784/638612875 C¹⁴
- 296 p(15): 289 - 27369371/45045 C + 2211965897/4729725 C² + 96579124871/70946875 C³
- 297 - 102420758777/30406375 C⁴ + 266410200482611/638612875 C⁵
- 298 - 296822434121761/91216125 C⁶ + 3609830350436851/212837625 C⁷
- 299 - 86845185235039/14189175 C⁸ + 33191885005374069/212837625 C⁹
- 300 - 45239444094237/16372125 C¹⁰ + 8443305704819099/2338875 C¹¹
- 301 - 57865626196623/1619125 C¹² + 58929797091794551/30405375 C¹³
- 302 - 801137232931268/12702876 C¹⁴ + 61062466535168/638612876 C¹⁵
- 303 p(16): -2 - 144 C² + 6720 C³ - 163720 C⁴ + 2040192 C⁵ - 17300976 C⁶ + 99418176 C⁷
- 304 - 401724180 C⁸ + 1167240680 C⁹ - 2485601424 C¹⁰ + 3788086948 C¹¹
- 305 + 4186351624 C¹² + 3240092800 C¹³ - 1666018800 C¹⁴ + 510975360 C¹⁵ - 70716340 C¹⁶
- 306 Degree of Faber polynomial: 18
- 307 p(0): -36
- 308 p(1): 594 - 568 C
- 309 p(2): -5952 + 10800 C - 4884 C²
- 310 p(3): 40455 - 105041 C + 92247 C² - 26625 C³
- 311 p(4): -197316 + 3309696/5 C - 8279004 C² + 2288912/5 C³ - 470688/5 C⁴
- 312 p(5): 712550 - 14284614/5 C + 22739904/5 C² - 1785768/5 C³ + 1408256 C⁴ - 1091472/5 C⁵
- 313 p(6): -1937620 + 310536350/35 C - 587009646/35 C² + 865976424/35 C³ - 325896904/35 C⁴
- 314 + 95420608/35 C⁵ - 11514976/35 C⁶

- 363 Degree of Faber polynomial: 19
- 364 p(0): -38
- 365 p(1): 665 - 627 C
- 366 p(2): -7106 + 38912/3 C - 17708/3 C²
- 367 p(3): 15832 - 137028 C + 120289 C² - 36055 C³
- 368 p(4): -273298 + 13912864/15 C - 3523360/3 C² + 9860848/15 C³ - 686014/5 C⁴
- 369 p(5): 1078103 - 21904093/5 C + 31693917/45 C² - 28470341/5 C³ + 6612166/3 C⁴
- 370 p(6): -16174681/45 C⁵
- 371 p(6): -3223380 + 105393968/7 C - 1016768736/35 C² + 1037666976/35 C³ - 5903444692/35 C⁴
- 372 + 36482880/7 C⁵ - 21991989/35 C⁶
- 373 p(7): 3437605 - 4034985607/105 C + 5324997988/63 C² - 32194596372/315 C³
- 374 + 26666916/35 C⁴ - 28022220/9 C⁵ + 327821516/45 C⁶ - 76541796/105 C⁷
- 375 p(8): -13123110 + 661963040/9 C - 1123568968/63 C² + 138068374688/567 C³
- 376 - 11637422040/567 C⁴ + 61882340320/567 C⁵ - 2894222272/81 C⁶ + 6329831456/81 C⁷
- 377 - 295548040/567 C⁸
- 378 p(9): 17809935 - 3692987319/35 C + 6844411362/25 C² - 71402478534/175 C³
- 379 + 67298279536/175 C⁴ - 8313090064/35 C⁵ + 3361290456/35 C⁶ - 4285766704/175 C⁷
- 380 + 6248265564/175 C⁸ - 396337876/175 C⁹
- 381 p(10): -18349630 + 389839940098/945 C - 529310011172/17325 C² + 8813446400736/14175 C³
- 382 - 112603020820/231 C⁴ + 17264720568944/51975 C⁵ - 4790019093924/31185 C⁶
- 383 + 2478084164096/51975 C⁷ - 491647791752/51975 C⁸ + 6769652512/6237 C⁹
- 384 - 2841321104/51975 C¹⁰
- 385 p(11): 14115100 - 8680033112/99 C + 358711332087/1485 C² - 8741483248471/22275 C³
- 386 + 27648431063208/66825 C⁴ - 397663122682/13365 C⁵ + 1108071286648/7425 C⁶
- 387 - 62908152752/1215 C⁷ + 74307352168/6075 C⁸ - 3777419032/2025 C⁹
- 388 + 198376492/1215 C¹⁰ - 381588172/66825 C¹¹
- 389 p(12): -7604468 + 104226307424/2145 C - 10065925442416/76075 C² + 161703318893616/76075 C³
- 390 - 57075272898/1365 C⁴ + 4165614616032/25025 C⁵ - 70732411576/825 C⁶
- 391 + 42809576704/1365 C⁷ - 7892386298/975 C⁸ + 33376375688/2275 C⁹ - 471281472/2275 C¹⁰
- 392 + 88468392/25025 C¹¹ - 13659208/2275 C¹²
- 393 p(13): 3105322 - 15040925426/819 C + 9169809427846/189189 C² - 42822319487422/567567 C³
- 394 + 13135780588340/1702701 C⁴ - 929872489282/1702701 C⁵ + 425647071153/154791 C⁶
- 395 - 24045858395/243243 C⁷ + 44548753492/187111 C⁸ - 770011100/11907 C⁹
- 396 + 5749104600/11907 C¹⁰ + 5259989260/11907 C¹¹ - 27493384160/130977 C¹²
- 397 + 2432268100/67567 C¹³
- 398 p(14): -810084 + 1216834868/273 C - 17038647331952/1576675 C² + 1097491563961984/709446675 C³
- 399 - 343105335461516376/364825 C⁴ + 1227515424876928/13050875 C⁵
- 400 - 134507122068090/30405375 C⁶ + 1317956405607584/70945875 C⁷
- 401 + 5415712405494/30405375 C⁸ + 57021875956730/16372125 C⁹
- 402 - 92676590112/166375 C¹⁰ + 3051313047488/486125 C¹¹ - 10141270163072/2338875 C¹²
- 403 + 17944038682016/10135125 C¹³ - 203081871987712/636512875 C¹⁴
- 404 p(15): 128877 - 88236867/143 C + 97813525069/76075 C² - 4185266641273/2627625 C³
- 405 + 1105709376593/875675 C⁴ - 168596736787/2627625 C⁵ - 18973465341/125125 C⁶
- 406 + 8752690414994/7137375 C⁷ - 499227093461/525625 C⁸ + 9893035940603/4156375 C⁹
- 407 - 1041360218672/125125 C¹⁰ + 1427849844922/202125 C¹¹ - 4475736748746/87375 C¹²
- 408 + 51004698718/125125 C¹³ - 73534333254/6005 C¹⁴ + 2065169470078/875875 C¹⁵
- 409 p(16): -10830 + 20764441472/51051 C - 96066948496/1461915 C² + 1463321678296/241215875 C³
- 316 p(7): 3896135 - 141441327/7 C + 302987673/7 C² - 356197519/7 C³ + 248017012/7 C⁴
- 317 - 14600340 C⁵ + 3294220 C⁶ - 2195692/7 C⁷
- 318 p(8): -6249100 + 237600576/7 C - 397626448/5 C² + 3670920768/35 C³ - 2872331624/35 C⁴
- 319 + 152062464/35 C⁵ - 48099584/5 C⁶ + 83804096/35 C⁷ - 1263824/7 C⁸
- 320 p(9): 735647 - 1465724798/35 C + 18272300096/175 C² - 23369694074/1575 C³
- 321 + 9992316356/75 C⁴ - 8205000956/105 C⁵ + 9418310528/315 C⁶ - 3773759488/525 C⁷
- 322 + 516615448/525 C⁸ - 91919456/1575 C⁹
- 323 p(10): -6418656 + 2057968752/85 C - 284222818868/275 C² + 10720476008/75 C³
- 324 - 1629586288/825 C⁴ + 71665167530/825 C⁵ - 2069002956/56 C⁶ + 26533689652/2475 C⁷
- 325 + 343518167/165 C⁸ - 24092368/2475 C⁹
- 326 p(11): 4065234 - 1288436154/55 C + 11707972036/1925 C² - 176753114934/1925 C³
- 327 + 17118437769/1925 C⁴ - 11298989819/1925 C⁵ + 51551887953/1925 C⁶
- 328 - 14756246501/175 C⁷ + 312647394/175 C⁸ - 6897412/25 C⁹ + 2359044/175 C¹⁰
- 329 + 1728092/1925 C¹¹
- 330 p(12): -131340544/13 C - 7587007584/3003 C² + 332958041536/9009 C³
- 331 - 950178621232/27027 C⁴ + 61805853056/27027 C⁵ - 21665300816/2079 C⁶
- 332 + 90870892192/27027 C⁷ - 1992033644/2457 C⁸ + 526472320/2457 C⁹
- 333 - 263436800/2457 C¹⁰ + 127124900/2457 C¹¹ - 314213920/27027 C¹²
- 334 p(13): 523260 - 275502116/1001 C + 224214764512/35035 C² - 463021858592/525525 C³
- 335 + 12064125800824/1576575 C⁴ - 2180654004952/4729725 C⁵ + 824325197312/429875 C⁶
- 336 - 280774641632/675875 C⁷ - 1769615002/4725 C⁸ + 31117587146/33075 C⁹
- 337 - 3985841176/33075 C¹⁰ + 349996947136/363825 C¹¹ - 158904017072/363825 C¹²
- 338 + 7413741608/67996 C¹³
- 339 p(14): -93024 + 43083176/1001 C - 11737846184/13475 C² + 892461130112/675875 C³
- 340 - 679393519584/675875 C⁴ + 52892752512/125125 C⁵ - 4477041936/125125 C⁶
- 341 + 970438394752/675875 C⁷ - 447743037344/125125 C⁸ + 55602979376/67375 C⁹
- 342 - 7660080028/6125 C¹⁰ + 915543476664/67375 C¹¹ - 86132620032/8925 C¹²
- 343 + 468528775168/125125 C¹³ - 560107893024/675875 C¹⁴
- 344 p(15): 8721 - 158438707/5005 C + 24083667413/525525 C² - 339952528757/7882875 C³
- 345 + 15316402041223/238875 C⁴ + 9409152794933/70945875 C⁵ - 11788770187293/10135125 C⁶
- 346 + 151171665839223/23648625 C⁷ - 114194996470991/4729725 C⁸
- 347 - 264186463512166/1819125 C⁹ - 219352337867543/1819125 C¹⁰ + 32254809890201/202125 C¹¹
- 348 + 336168298452694/70945875 C¹² + 1450502279842/1625 C¹³ - 429984517698466/14189175 C¹⁴
- 349 + 336168298452694/70945875 C¹⁵
- 350 p(16): -324 + 59580288/85085 C - 1897958752/2877975 C² + 33535776128/14889875 C³
- 351 - 1853683284/328825 C⁴ + 1836317044048/28801775 C⁵
- 352 - 6722582886728/10664325 C⁶
- 353 + 3430758411051328/2727375 C⁷ - 3862020211849512/23648625 C⁸
- 354 + 652947641816986/134008875 C⁹ - 415811276671138692/402028625 C¹⁰
- 355 + 1451941028286576/893575 C¹¹ - 579246595067619636/30925125 C¹²
- 356 + 181733692471856/12182625 C¹³ - 24356651056126336/30925125 C¹⁴
- 357 + 2866669715918016/120607875 C¹⁵ - 422987030277632/120607875 C¹⁶
- 358 p(17): 2 + 2 C - 160 C² + 218680 C³ - 218680 C⁴ + 3285128 C⁵ - 31691988 C⁶ + 208657472 C⁷
- 359 - 973077820 C⁸ + 3300860420 C⁹ - 8257854176 C¹⁰ + 16319161312 C¹¹
- 360 + 21000475496 C¹² + 20976010200 C¹³ - 148343227200 C¹⁴ + 7031994240 C¹⁵
- 361 - 2003601300 C¹⁶ + 259299580 C¹⁷
- 362

410	-	13935480228072/278326125 C ⁴ + 2636208921379744/10854718875 C ⁵
411	P(13):	14858000 - 2881072965440/3003 C + 5850074791936/21021 C ² - 1679966303376/35035 C ³
412	-	12899541893931616/212837625 C ⁸ + 87118850764608/4386745 C ⁹
413	-	1570461000529832368/361823925 C ¹⁰ + 6018879922969984/8434125 C ¹¹
414	-	233659249412910576/278326125 C ¹² + 9225889276946416/134008875 C ¹³
415	-	4054511906411824192/10854718875 C ¹⁴ + 20112005230822784/16695675 C ¹⁵
416	-	63186274333638772/361823925 C ¹⁶
417	P(17):	361 - 617007473/766765 C + 15934000508/241216975 C ² + 2606505890989/1206079875 C ³
418	-	745262986651664/10854718875 C ⁴ + 11842675683618664/10854718875 C ⁵
419	-	10554600839521903366/97692469875 C ⁶ + 747529481471779744/97692469875 C ⁷
420	-	28011030496730376/7514806375 C ⁸ + 85643060039006076262/6512831325 C ⁹
421	-	6532706038911073944/191536825 C ¹⁰ + 250567813244648004/363107725 C ¹¹
422	-	272427142569193312/29469825 C ¹² + 3639732211702782112/383107725 C ¹³
423	-	13213471927375623504/191536825 C ¹⁴ + 192599314147323136304/5746618875 C ¹⁵
424	-	56156740049206840822/5746618875 C ¹⁶ + 1263292974632668146/97692469875 C ¹⁷
425	-	2 - 180 C ² + 10560 C ³ - 304920 C ⁴ + 5144832 C ⁵ - 55979616 C ⁶ + 417668128 C ⁷
426	-	22251465760 C ⁸ + 86927478080 C ⁹ - 25323493624 C ¹⁰ + 56506864048 C ¹¹
427	-	91677435304 C ¹² + 113388729600 C ¹³ - 103272796800 C ¹⁴ + 67206706560 C ¹⁵
428	-	29547846540 C ¹⁶ + 7860568320 C ¹⁷ - 955277400 C ¹⁸
429	Degree of Faber polynomial:	20
430	P(0):	40
431	P(1):	740 - 700 C
432	P(2):	68400 + 46240/3 C - 21160/3 C ²
433	P(3):	65460 - 523010/3 C + 462790/3 C ² - 136010/3 C ³
434	P(4):	-371008 + 1272000 C - 1628048 C ² + 921728 C ³ - 194712 C ⁴
435	P(5):	1582240 - 19681472/3 C + 96382016/9 C ² - 8732448 C ³ + 10613260/3 C ⁴ - 5125148/9 C ⁵
436	P(6):	-5178240 + 172147456/7 C - 3044208704/63 C ² + 3166360208/63 C ³ - 204224640/7 C ⁴
437	P(7):	564327392/63 C ⁵ - 71563640/63 C ⁶
438	-	13147875 - 487308235/7 C + 10962749337/7 C ² - 1357702795/7 C ³ + 999241413/7 C ⁴
439	-	62401197 C ⁵ + 14993587 C ⁶ - 10686891/7 C ⁷
440	-	-26013000 + 9432501760/63 C - 23504864384/63 C ² + 237926766080/567 C ³
441	-	269215693152/567 C ⁴ + 20369898752/81 C ⁵ - 6913639040/81 C ⁶
442	-	925973962/567 C ⁷ - 109164704/81 C ⁸
443	-	40069020 - 209802108/9 C + 13947862016/21 C ² - 578515648000/567 C ³
444	-	27022520480/27 C ⁴ - 121898994208/189 C ⁵ + 154700422764/567 C ⁶ - 1971146856/27 C ⁷
445	-	2117216048/169 C ⁸ - 426503686/567 C ⁹
446	-	147290400 + 335493936/11 C - 33262516962/385 C ² + 48987550464/35 C ³
447	-	1674589976/11 C ⁴ + 42105438796/385 C ⁵ - 41250213447/77 C ⁶ + 9705981696/55 C ⁷
448	-	1439199004/385 C ⁸ + 353712512/77 C ⁹ - 13466824/55 C ¹⁰
449	-	434596560 - 6571413362/231 C + 1234272951058/1485 C ² - 14685849907282/10395 C ³
450	-	300544685121056/187111 C ⁴ + 3653265518768/13365 C ⁵ + 593044447264/8910 C ⁶
451	-	2125640977184/8505 C ⁷ + 545301906488/8505 C ⁸ - 6000783032/567 C ⁹
452	-	8848445656/8505 C ¹⁰ - 118943656/2673 C ¹¹
453	-	209716000 + 251407903040/1287 C - 22222893705808/3861 C ² + 5200344436544/5265 C ³
454	-	-20072058686232/173745 C ⁴ + 159966147798016/173745 C ⁵ - 6961899934976/13365 C ⁶
455	-	36659373654272/173745 C ⁷ - 952178080192/15795 C ⁸ + 188302748672/15795 C ⁹
456	-	
457	-	24602414656/15795 C ¹⁰ + 22278312448/173745 C ¹¹ - 180424672/173745 C ¹²
458	-	14858000 - 2881072965440/3003 C + 5850074791936/21021 C ² - 1679966303376/35035 C ³
459	-	12899541893931616/212837625 C ⁸ + 87118850764608/4386745 C ⁹
460	-	1570461000529832368/361823925 C ¹⁰ + 6018879922969984/8434125 C ¹¹
461	-	233659249412910576/278326125 C ¹² + 9225889276946416/134008875 C ¹³
462	-	4054511906411824192/10854718875 C ¹⁴ + 20112005230822784/16695675 C ¹⁵
463	-	63186274333638772/361823925 C ¹⁶
464	-	32171044000/1702701 C ⁴ + 2064815448940/243243 C ⁸ + 409884351232/130977 C ⁹
465	-	4611073025625424/1702701 C ⁴ + 2064815448940/243243 C ⁸ + 409884351232/130977 C ⁹
466	-	32171044000/1702701 C ⁴ + 2064815448940/243243 C ⁸ + 409884351232/130977 C ⁹
467	-	29829023424/34748 C ¹³ - 811541290592/5108103 C ¹⁴
468	-	19225786 - 1922281015/673 C + 5880389148731/315315 C ² - 377183221613537/41189175 C ³
469	-	968674623169/363825 C ⁴ - 321570889391/18943225 C ⁵
470	-	16286796276817/18245225 C ⁹ - 1019202664455687/42567525 C ⁷ - 38645558974/135135 C ⁸
471	-	412241232739223969775 C ⁹ - 7201141828665673274426 C ¹⁰ + 9318933096314/297875 C ¹¹
472	-	67812203043067227275 C ¹² + 16739343803654/968725 C ¹³ - 18256199846165425540615 C ¹⁴
473	-	21492290408702/18243225 C ¹⁵
474	-	175560 + 191816966/221 C - 484008543808/255255 C ² + 21646251170816/8933925 C ³
475	-	11192613024/5525 C ⁴ + 11086499244544/8933925 C ⁵ - 11100063116608/8933925 C ⁶
476	-	6874201501696/1276275 C ⁷ - 824161510768/35035 C ⁸ + 68990501278208/8933925 C ⁹
477	-	1827227411499136/8933925 C ¹⁰ + 30445613106686/98175 C ¹¹
478	-	25894908235584/687225 C ¹² + 94814945974208/2977975 C ¹³ - 3022377816960/17017 C ¹⁴
479	-	17500405643264/2977975 C ¹⁵ - 1039838588496/119119 C ¹⁶
480	-	1124344180/21879 C ⁴ + 117909439616/1378377 C ² - 740834218258272/2170943775 C ⁵
481	-	7533282554355904/1953849375 C ⁶ + 78202826023555648/2791213425 C ⁷
482	-	27848486194936153507/1953849375 C ⁸ + 3409048478270101384/6512831325 C ⁹
483	-	53948336103911192/383107725 C ¹⁰ + 152870157933427486/383107725 C ¹¹
484	-	120047660297113376/29469825 C ¹² + 165106697628078496/383107725 C ¹³
485	-	176937244278044544/54729875 C ¹⁴ + 18406488706817632/1495233175 C ¹⁵
486	-	549503514111406284/1493233175 C ¹⁶ + 18040222167739936/2791213425 C ¹⁷
487	-	400 + 2638134660/2909907 C - 1115194312/1281887 C ² + 318246900608/916620705 C ³
488	-	50793506890944/53687425 C ⁴ + 3321845185741686/1964187225 C ⁵
489	-	146711533964942336/7576150725 C ⁶ + 18726123780816574206/123743795175 C ⁷
490	-	1040503939952743872/123743795175 C ⁸ + 1267440688517981857472/371231386525 C ⁹
491	-	850177681830755696/824958345 C ¹⁰ + 1155812923161639366/49517325 C ¹¹
492	-	826478346843764544/207972765 C ¹² + 3186518208089368/6302205 C ¹³
493	-	22939649081405610432/485265785 C ¹⁴ + 688469443876941236528/21837140325 C ¹⁵
494	-	103243365136464150433/7729048775 C ¹⁶ + 47709286908281668672/123743795175 C ¹⁷
495	-	253578494962002352/5303360375 C ¹⁸
496	-	2 + 2 C - 198 C ² + 13002 C ³ - 417648 C ⁴ + 7861392 C ⁵ - 95758664 C ⁶ + 803451792 C ⁷
497	-	4840020900 C ⁸ + 21530739490 C ⁹ + 7206214498 C ¹⁰ + 18353186292 C ¹¹
498	-	374245453468 C ¹² + 531495624440 C ¹³ - 598282925760 C ¹⁴ + 500719348460 C ¹⁵
499	-	301742355780 C ¹⁶ + 123681129660 C ¹⁷ - 30855460020 C ¹⁸ + 3534526380 C ¹⁹